Appendix A: FEM verification

The goal of this appendix is to validate the structural performance of a solution selected from the Pareto fronts of Fig. 6 by using the Ansys® software. Indeed, we select the solution that corresponds to minimum reliability in cluster 6 (indicated by a red point in Fig. 6). First, by using Eq. (57), we can deduce the reliability of the two products (Machine A, Machine B). We then consider the second product (Machine B) whose characteristics are $R^{1}_{\text{product}}=0.5027$ and $R^{2}_{\text{product}}=0.5$ respectively. After that, by using the Ansys® Workbench tool, we verified structural performances for the gear pair, pinion and gearwheel shafts: the dedendum bending strength, surface contact strength and Von Mises stress. These results are compared with those given by the ISO standard and the ASME code.

The FEM based study is performed as follows. In SolidWorks 2015, 3D-CAD models of gear pair, pinon and gearwheel shafts are built based on the geometry data of the selected solution. The involute tooth profile is created by using "Equation Driven Curve" in SolidWorks. The geometric models are then imported directly into Ansys Workbench 16, without losing accuracy, via a bidirectional interface. The gear finite element model includes five teeth for the gearwheel and five teeth for the pinion. The middle pinon tooth is at the beginning of the mesh in the model configuration, it represents the target tooth in static analysis in order to determinate the bending and contact stress (Fig. 7a). The finite element models of the pinion and gearwheel shafts are also built by including keyway dimensions that are designed in accordance to the ISO standard. Due of the model symmetry, only a half part of the shaft is considered in static analysis (Fig. 7b). In Ansys Workbench, we created two static structural analyses: the first evaluates the bending and contact stress of the gear pair (Fig. 8a) and the second evaluates the Von Mises stress of the pinion and gearwheel shafts (Fig. 8b).

The data used in the finite element analysis and the results of two static structural analyses are summarized in Tables 9 and 10. Fig. 9 illustrates some selected FEM results. Globally, we noticed that the numerical results predicted by analytical formulas employed during the optimization process, particularly the ISO standard for gears and the ASME code for shafts, are in good agreement with those given by FEM using the Ansys ® software.

Nomenclature

| Р | Transmitted power (W) | Z_W | Work harden coefficient |
|-------------------|--|--------------------|--|
| и | Gear ratio | Z_X | Size coefficient |
| α | Pressure angle (degree) | | $_n$ Experimental gear bending fatigue strength(N/m ²) |
| β | Helix angle (degree) | $o_{H lin}$ | m Experimental gear contact fatigue strength (N/m^2) |
| а | Distance center (mm) | σ_{uts} | Ultimate tensile strength (N/m ²) |
| m_n | Normal module (mm) | $K_{H\beta}$ | Longitudinal load distribution coefficient |
| D_1^{n} | Pinion pitch diameter (mm) | $K_{H\alpha}$ | Transverse load distribution coefficient |
| D_2 | Gearwheel pitch diameter (mm) | K_V | Dynamic load coefficient |
| d_{a1} | Pinion shaft diameter (mm) | K_A | Work condition coefficient |
| d_{a2} | Gearwheel shaft diameter (mm) | $K_{F\beta}$ | Longitudinal load distribution coefficient |
| F_t | Rated tangential tooth force at transverse pitch (N) | $K_{F\alpha}$ | Transverse load distribution coefficient |
| N_1 | Rotation speed (rmp) | Y_{β} | Helix angle coefficient |
| Z_{β} | Helix angle coefficient | $Y_{\mathcal{E}}$ | Contact ratio factor |
| Z_{ε} | Contact ratio coefficient | Y_{NT} | Life coefficient |
| Z_H | Nodal field coefficient | $Y_{S\alpha}$ | Dedendum stress concentration coefficient |
| Z_N | Life coefficient | Y_X | Size coefficient |
| Z_L | Lubricant coefficient | $Y_{\delta rel}$ | T Relative sensitive coefficient |
| Z_V | Velocity coefficient | $Y_{F\alpha}$ | Tooth form factor |
| Z_R | Tooth fineness coefficient | Y _{Rrel1} | Relative surface condition coefficient |
| Z_E | Elastic coefficient | Y_{ST} | Experimental gear dedendum stress concentration coefficient |
| MOOP | Multi-Objective Optimization Problem | DIN | Deutsches Institut für Normung |
| ASME | American Society of Mechanical Engineers | SKF | Svenska KullagerFabriken |
| ISO | International Organization for Standardization | AGMA | A American Gear Manufacturers Association |
| NSGA-I | I Non-dominated Sorting Genetic Algorithm | | |

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|---|------|------|------|--|
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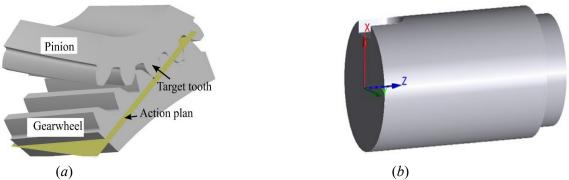
| Material | 42CrMo4 | |
|------------------|----------------------------------|----------------------------|
| Common geometric | Normal module (mm) =3.5 | Width (mm)= 28.021 |
| parameters | Normal pressure angle(deg)=20 | Helix angle (deg)= 15 |
| | Contact ratio=2.115 | |
| Pinion | Number of teeth | 22 |
| | Speed (rpm) | 1150 |
| | Torque (Nm) | 124.556 |
| Gearwheel | Number of teeth | 77 |
| | Speed (rpm) | 328.57 |
| | Torque (Nm) | 435.946 |
| Connections | Contact | Five pinion tooth surfaces |
| | Target | Five wheel tooth surfaces |
| | Contact Type | Frictionless |
| | Formulation | Augmented Lagrange |
| | Penetration Tolerance Value | 1E-3mm |
| | Update Stiffness | Each Iteration |
| | Interface Treatment | Adjust to Touch |
| | Joints (Pinion - Gearwheel hubs) | Body-Ground Revolute joint |
| Mesh | Physic preference | CFD |
| | Element order | Quadratic |

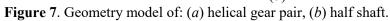
 Table 9. Main parameters of the gear pair and the associate FEM study

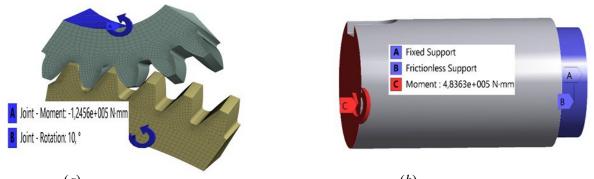
| | Method | Sweep | | |
|--|--|--------------------------------------|--|--|
| | Sweep Number Division | 20 | | |
| | Pinion and Gearwheel sizing | 1mm | | |
| | Contact surfaces and root teeth sizing | 0.15mm | | |
| Total number of nodes | | 432962 | | |
| | Total number of elements | 115024 | | |
| Analysis setting | Auto Time stepping | On | | |
| | Initial Substeps | 80 | | |
| | Minimum Substeps | 80 | | |
| | Maximum Substeps | 100 | | |
| | Large Deflection | On | | |
| Loads and Supports | Joint- Moment | Joint Revolute - Ground to pinon | | |
| (see Fig. 8a) | DOF | Rotation Z | | |
| | Magnitude | Tabular Data (-124.556Nm) | | |
| | Joint- Rotation | Joint Revolute - Ground to Gearwheel | | |
| | DOF | Rotation Z | | |
| | Magnitude | 10 degree | | |
| Comparison between FEM and ISO results | | | | |
| Dedendum bending | FEM: 142.37 MPa | ISO: 166.56 MPa | | |
| stress | | | | |
| Surface contact | FEM: 729.33 MPa | ISO: 706.88 MPa | | |
| stress | | | | |

Table 10. Main parameters of the shafts and the associate FEM study

| Material | 25CrMo4 | | | |
|---|--|----------------------------|--|--|
| Pinion shaft | Diameter | 46.32 mm | | |
| | Length | 200 mm | | |
| | Speed | 1150 rpm | | |
| | Torque | 124.556 Nm | | |
| Gearwheel shaft | Diameter | 51.07 mm | | |
| | Length | 200 mm | | |
| | Speed | 328.57 rpm | | |
| | Torque | 435.946 Nm | | |
| Mesh | Method | Hex Dominant | | |
| | Body sizing | 2mm | | |
| | Fillet keyway sizing | 0.2 mm | | |
| | Total number of nodes (half pinion) | 509182 | | |
| | Total number of nodes (half shaft) | 1028104 | | |
| | Total number of elements (half pinion) | 148973 | | |
| | Total number of elements (half shaft) | 300775 | | |
| Loads and Supports | Fixed supports | Frictionless Support | | |
| (see Fig. 8 <i>b</i>) | Pinion shaft moment | X component = -74.933 Nm | | |
| | | Y component = 198.860 Nm | | |
| | | Z component = 124.556 Nm | | |
| | Gearwheel shaft moment | X component= -74.933 Nm | | |
| | | Y component = 198.860 Nm | | |
| | | Z component = 435.946 Nm | | |
| Comparison between FEM and ASME results | | | | |
| Von Mises stress - | FEM: 82.35 MPa | ASME: 93.574 MPa | | |
| pinon shaft | | | | |
| Von Mises stress - | FEM: 126.69 MPa | ASME: 132.58 MPa | | |
| gearwheel shaft | | | | |







(a) (b) Figure 8. FEM loads and supports: (a) two joints applied on hubs, (b) boundary conditions.

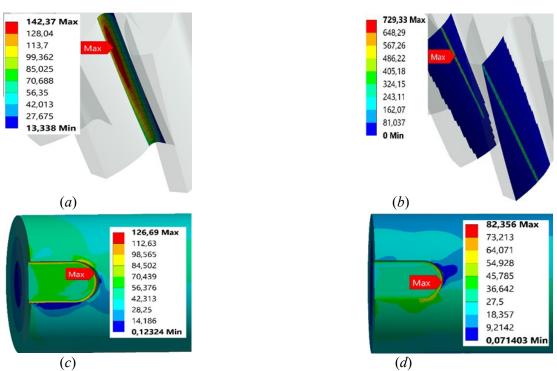


Figure 9. FEM Results: (a) bending stress, (b) contact stress, (c) gearwheel shaft (d) pinion shaft.